Results of Proficiency Test Turbine Oil (used) May 2018

Organised by: Institute for Interlaboratory Studies Spijkenisse, the Netherlands

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1 Introduction

Since 2013, the Institute for Interlaboratory Studies (iis) organizes a proficiency test for used Turbine Oil. During the annual proficiency testing program 2017/2018, it was decided to continue the round robin for the analysis of used Turbine Oil. In this interlaboratory study 43 laboratories in 31 different countries registered for participation. See appendix 2 for the number of participants per country. In this report, the results of the 2018 used Turbine Oil proficiency test are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, The Netherlands, was the organizer of this proficiency test (PT). Sample analyses for fit-for-use and homogeneity were subcontracted to an ISO/IEC 17025 accredited laboratory. It was decided to send one bottle of 1L (labelled #18077) of used Turbine Oil.

The participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC 17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). This PT falls under the accredited scope. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

2.2 PROTOCOL

The protocol followed in the organization of these proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organization, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

The necessary bulk material of used Turbine Oil was obtained from a third party. The 60 litre bulk material was homogenized and 49 amber glass bottles of 1 litre were filled and labelled #18077. The homogeneity of the subsamples #18077 was checked by determination of Density at 15°C in accordance with ASTM D4052 on 8 stratified randomly selected samples.

| | Density at 15°C in kg/m³ |
|-----------------|-----------------------------|
| Sample #18077-1 | 959.98 |
| Sample #18077-2 | 960.00 |
| Sample #18077-3 | 959.98 |
| Sample #18077-4 | 960.05 |
| Sample #18077-5 | 959.99 |
| Sample #18077-6 | 960.03 |
| Sample #18077-7 | 959.99 |
| Sample #18077-8 | 960.04 |

Table 1: homogeneity test results of subsamples #18077

From the above test results, the repeatability was calculated and compared with 0.3 times the corresponding reproducibility in agreement with the procedure of ISO 13528, Annex B2 in the next table:

| | Density at 15°C in kg/m³ |
|--------------------------------|-----------------------------|
| r(observed) | 0.08 |
| reference test method | ASTM D1298:12b(2017) |
| 0.3 x R(reference test method) | 0.45 |

Table 2: evaluation of the repeatabilities of the subsamples #18077

The calculated repeatability was in agreement with 0.3 times the corresponding reproducibility of the reference test method. Therefore, homogeneity of the subsamples #18077 was assumed.

To each of the participating laboratories, one sample of 1 L amber glass bottle (labelled #18077) was sent on April 25, 2018.

2.5 STABILITY OF THE SAMPLES

The stability of the Turbine Oil (used), packed in the amber glass bottles, was checked. The material was found sufficiently stable for the period of the proficiency test.

2.6 ANALYSES

The participants were requested to determine on sample #18077: Acid Number, Color ASTM, Density at 15°C, Flash Point (COC & PMcc), Insoluble Color Bodies, Kinematic Viscosity at 40°C and at 100°C, Viscosity Index, Oxidation Stability RPVOT, Water by KF, Water separability, Steam Demulsibility Characteristics, Steam Water Separation Ability and Level of contamination (parts per ml and ISO Class).

Also, some additional questions were requested about Acid Number (method ASTM D664).

It was explicitly requested to treat the sample as if it was a routine sample and to report the test results using the indicated units on the report form and not to round the results, but report as much significant figures as possible. It was also requested not to report 'less than' results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

To get comparable test results, a detailed report form and a letter of instructions are prepared. On the report form, the reporting units are given as well as the reference test methods that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the participants were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment.

Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalyses). Additional or corrected test results are used for data analysis and original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the (results of the) statistical evaluation should be used with due care.

According to ISO 5725 the original test results per determination were submitted to Dixon's, Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1, was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualise the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis.

The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve was projected over the Kernel Density Graph for reference.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation in this interlaboratory study. The target standard deviation was calculated from the literature reproducibility by division with 2.8.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

```
z_{\text{(target)}} = (test result - average of PT) / target standard deviation
```

The z_(target) scores are listed in the result tables in appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare.

The usual interpretation of z-scores is as follows:

```
|z|<1 good

1 < |z| < 2 satisfactory

2 < |z| < 3 questionable

3 < |z| unsatisfactory
```

4 EVALUATION

In this interlaboratory study, no problems were encountered with the dispatch of the samples to laboratories. All participating laboratories reported test results, but not all laboratories were able to report all analyses requested. In total 43 participants reported 581 test results. Observed were 10 outlying results, which is 1.7% of the numerical results. In proficiency studies, outlier percentages of 3% - 7.5% are guite normal.

4.1 **EVALUATION PER TEST**

In this section, the results are discussed per test. The methods, which are used by the various laboratories, are taken into account for explaining the observed differences when possible and applicable. These methods are also in the tables together with the original data. The abbreviations, used in these tables, are listed in appendix 3.

In the iis PT reports, ASTM methods are referred to with a number (e.g. D1500) and an added designation for the year that the method was adopted or revised (e.g. D1500:12). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D1500:12(2017). In the results tables of Appendix 1 only the method number and year of adoption or revision e.g. D1500:12 will be used.

Not all original data sets proved to have a normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

Acid Number:

This determination was very problematic. No statistical outliers were observed. However, the calculated reproducibility is not at all in agreement with the requirements of ASTM D664:17a, method A (both Buffer End Point pH 11 and the less strict Inflection Point).

Method ASTM D664 states in paragraph 13.1.2: "For all acid titrations on used oils, mark as an end point the point on the curve that corresponds to the meter reading for an aqueous basic buffer (pH 11)." Remarkably, of all the laboratories that reported a selection of the end point, around fifty percent reported to have used the Inflection Point instead of the Buffer End Point (BEP). When evaluating the results using the Inflection Point and the BEP separately, the calculated reproducibility for using a determination with BEP is still not in agreement with the requirements of ASTM D664:17a, method A (BEP pH 11), but the calculated reproducibility for using a determination with Inflection Point is in agreement with the less strict requirements of ASTM D664:17a, method A (Inflection Point). The volume of titration solvent used did not appear to have an influence.

Color ASTM:

This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with ASTM D1500:12(2017).

Density at 15°C:

This determination was not problematic. Three statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D1298:12b(2017).

<u>Flash Point COC</u>: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ASTM D92:16b.

Flash Point PMcc: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D93:16a, procedure A. When evaluated separately for procedure A and procedure B, the respective calculated reproducibilities are also in agreement with the respective methods.

Insoluble Color Bodies: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D7843:16.

Kin.Visco.at 40°C: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the estimated reproducibility based on the reproducibilities as observed in a large number of iis PTs on used oils (lit. 16). The kinematic viscosity is lower than the range that is mentioned in ASTM D445:17a (25-125 mm²/s), therefore the strict requirements of ASTM D445:17a were not used.

Kin.Visco.at 100°C: This determination was problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is not in agreement with the estimated reproducibility based on the reproducibilities as observed in a large number of iis PTs on used oils (lit. 16). The kinematic viscosity is lower than the range that is mentioned in ASTM D445:17a (6-16 mm²/s), therefore the strict requirements of ASTM D445:17a were not used.

Viscosity Index

This determination was problematic. One statistical outlier was observed and one other test result was excluded. Since the performance of the kinematic viscosity test at 40°C and 100°C was calculated using the target reproducibility based on iis historical data (lit. 16) and not against the very strict requirements of ASTM D445, the larger variation present in these data sets will give more variation in the results of the Viscosity Index calculation. Therefore, no z-scores were calculated.

From the test results reported for kinematic viscosity at 40°C and at 100°C, iis calculated the Viscosity Indices and compared the results with the reported Viscosity Indices. Four participants did not calculate the VI index correctly. A separate statistical evaluation was done on the group of (iis) calculated viscosity indices. No improvement was found for the resulting calculated reproducibility of the group.

Oxidation Stability RPVOT: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ASTM D2272:14a.

Water by KF:

This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D6304:16e1.

Water separability: This determination was not problematic. No statistical outliers were observed. All reporting laboratories, except one, reported a complete break of (40-40-0) or emulsion less than 3 ml. The calculated reproducibilities for time to reach 3 ml or less emulsion, time to reach 37 ml of water and time to reach complete break (40-40-0) are all in agreement with the requirements of ASTM D1401:18a.

Steam Demulsibility Char.: Only three participants reported a result between 76 and 120 seconds. No z-scores were calculated.

Steam Water Separation Ability.: Only one participant reported a result of 79 seconds. No zscores were calculated.

Level of Contamination: This determination was problematic. No statistical outliers were observed and eight test results were excluded. The calculated reproducibilities for number of particles in counts/ml for ≥4µm, ≥6µm and ≥14µm after rejection of the suspect data are not in agreement with the requirements of ASTM D7647:10(2018).

> This determination was also problematic for the test results reported in ISO scale numbers. Three statistical outliers were observed and eight other test results were excluded. The calculated reproducibilities for number of particles in ISO scale numbers ≥6µm and ≥14µm after rejection of the suspect data are not in agreement with the requirements of ASTM D7647:10(2018). The calculated reproducibility in ISO scale numbers for ≥4µm is in good agreement with the requirements of ASTM D7647:10(2018).

4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the relevant reference test method and the reproducibility as found for the group of participating laboratories that participated. The average results, calculated reproducibilities and reproducibilities derived from reference test methods (for example ASTM or IP standards), are compared in the next table.

| parameter | unit | n | average | 2.8 * sd | R(lit) |
|---------------------------------------|-----------|----|---------|----------|--------|
| Acid Number, total | mg KOH/g | 37 | 0.19 | 0.19 | 0.09 |
| Color ASTM | | 17 | 3.6 | 0.6 | 1 |
| Density at 15°C | kg/m³ | 39 | 959.9 | 0.8 | 1.5 |
| Flash Point COC | °C | 29 | 224 | 24 | 18 |
| Flash Point PMcc | °C | 37 | 188 | 11 | 13 |
| Insoluble Color Bodies | | 11 | 15.9 | 7.3 | 9.2 |
| Kinematic Viscosity at 40°C | mm²/s | 37 | 12.78 | 0.15 | 0.23 |
| Kinematic Viscosity at 100°C | mm²/s | 36 | 3.20 | 0.08 | 0.07 |
| Viscosity Index | | 31 | 116 | 12 | (2) |
| Oxidation Stability RPVOT | minutes | 16 | 802 | 305 | 183 |
| Water by KF | mg/kg | 34 | 933 | 320 | 1022 |
| Water Separability at 54°C | | | | | |
| - Time to reach 3 ml or less emulsion | minutes | 16 | 6 | 5 | 20 |
| - Time to reach 37 of water | minutes | 15 | 6 | 5 | 20 |
| - Time to reach complete break | minutes | 14 | 7 | 7 | 20 |
| Demulsibility Characteristics, Steam | S | 3 | 76-120 | n.e | n.e. |
| Water Separation Ability, Steam | S | 1 | 79 | n.e. | n.e. |
| Level of Contamination ≥4µm (c) | counts/ml | 22 | 20235 | 28165 | 22866 |
| Level of Contamination ≥6µm (c) | counts/ml | 24 | 4561 | 6908 | 3466 |
| Level of Contamination ≥14µm (c) | counts/ml | 21 | 176 | 302 | 238 |
| Level of Contamination ≥4µm (c) | ISO scale | 22 | 22 | 2 | 2 |
| Level of Contamination ≥6µm (c) | ISO scale | 27 | 19 | 3 | 1 |
| Level of Contamination ≥14µm (c) | ISO scale | 24 | 15 | 3 | 2 |

Table 3: reproducibilities of tests of sample #18077

Without further statistical calculations it can be concluded that for a number of tests there is a good compliance of the group of participants with the relevant reference test methods. The tests that are problematic have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF MAY 2018 WITH PREVIOUS PTs

| | May 2018 | May 2017 | May 2016 | May 2015 | May 2014 |
|----------------------------|----------|----------|----------|----------|----------|
| Number of reporting labs | 43 | 34 | 38 | 39 | 29 |
| Number of results reported | 581 | 508 | 474 | 398 | 301 |
| Statistical outliers | 10 | 16 | 15 | 36 | 10 |
| Percentage outliers | 1.7% | 3.1% | 3.2% | 9.0% | 3.3% |

Table 4: comparison with previous proficiency tests

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared to the requirements of the respective reference test methods. The conclusions are given in the following table:

| Determination | May 2018 | May 2017 | May 2016 | May 2015 | May 2014 |
|------------------------------|----------|----------|----------|----------|----------|
| Acid Number, total | | - | - | + | |
| Color ASTM | + | + | +/- | + | ++ |
| Density at 15°C | + | + | ++ | ++ | +/- |
| Flash Point COC | - | + | () | n.e. | n.e. |
| Flash Point PMcc | + | + | +/- | +/- | - |
| Insoluble Color Bodies | + | - | +/- | n.e. | n.e. |
| Kinematic Viscosity at 40°C | + | - | ++ | ++ | ++ |
| Kinematic Viscosity at 100°C | +/- | | +/- | + | +/- |
| Viscosity Index | () | | | | |
| Oxidation Stability RPVOT | - | - | ++ | n.e. | n.e. |
| Water by KF | ++ | ++ | ++ | ++ | ++ |
| Water Separability | ++ | ++ | n.e. | + | n.e. |
| Level of Contamination ≥4µm | - | - | | | n.e. |
| Level of Contamination ≥6µm | | | | | n.e. |
| Level of Contamination ≥14µm | - | - | - | | n.e. |

Table 5: comparison determinations against the standard

The performance of the determinations against the requirements of the respective reference test methods is listed in the above table. The following performance categories were used:

++: group performed much better than the reference test method

+ : group performed better than the reference test method

+/-: group performance equals the reference test method

- : group performed worse than the reference test method

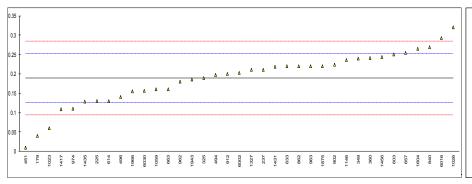
-- : group performed much worse than the reference test method

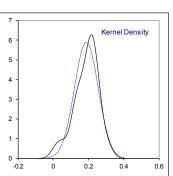
n.e.: not evaluated

APPENDIX 1

Determination of Acid Number (total) on sample #18077; results in mg KOH/g

| lah | method | value | mark | z(tara) | determination of end point | volume of titration solvent |
|------|--|---------|---------|----------|----------------------------|--------------------------------|
| | D664Mod. | <0.10 | IIIai K | <u> </u> | | |
| | D664-A | 0.04 | | | Buffer End Point (pH 11) | 60 mL |
| | D974 | 0.04 | | -1.86 | , | |
| | D664-A | 0.13 | | 0.69 | | |
| | D664-A | 0.211 | | | Buffer End Point (pH 11) | 125 mL |
| 331 | D004-A | 0.19 | | | | 125 IIIL |
| | D664-A | 0.24 | | | Inflection Point | 125 mL |
| | D664-A | 0.24 | | | Inflection Point | 60 mL |
| 432 | D004-A | 0.241 | | | | |
| | In house | 0.01 | | -5.64 | | |
| | D664-A | 0.01 | | | Inflection Point | 125 mL |
| | | | | | | |
| 541 | D664-A | 0.14 | | -1.55 | Buffer End Point (pH 11) | 60 mL |
| | D664 A | | | | Inflaction Daint | |
| | D664-A | 0.2498 | | | Inflection Point | 125 mL |
| | D974 | 0.13 | | -1.86 | | 60 mL |
| | D664-A | 0.22 | | | Inflection Point | 125 mL |
| | D664-A | 0.254 | | | | 405 |
| | D664-A | 0.1605 | | | Buffer End Point (pH 11) | 125 mL |
| | D664-A | 0.269 | | | Inflection Point | 125 mL |
| | D664-A | 0.22 | | 0.98 | | |
| | D664-A | 0.224 | | | Buffer End Point (pH 11) | 60 mL |
| | D664-A | 0.20 | | 0.34 | | |
| | D974 | 0.18 | | -0.29 | | |
| | D664-A | 0.22 | | | Inflection Point | 60 mL |
| | D664-A | 0.11 | | -2.49 | | 60 mL |
| 1017 | | | | | | |
| | In house | 0.06 | | -4.07 | | |
| 1026 | D664-A | 0.32 | | 4.13 | | |
| | ISO6619 | 0.16 | | | Buffer End Point (pH 11) | 60 mL |
| 1146 | D664-A | 0.235 | | | Buffer End Point (pH 11) | 125 mL |
| 1327 | D664-B | 0.21 | | | Buffer End Point (pH 11) | 60 mL |
| 1417 | D664-A | 0.109 | | -2.52 | Buffer End Point (pH 11) | 125 mL |
| 1431 | D664-A | 0.2183 | | 0.92 | Inflection Point | 60 mL |
| 1435 | D664-A | 0.129 | | -1.89 | Buffer End Point (pH 11) | |
| 1456 | D974 | 0.2433 | | 1.71 | | 125 mL |
| 1604 | D664-A | 0.2646 | | 2.38 | | |
| 1875 | ISO6618 | 0.22 | | 0.98 | Inflection Point | 60 mL |
| 1943 | ISO6618 | 0.185 | | -0.13 | | |
| 1966 | ISO6618 | 0.1548 | | -1.08 | | |
| 6002 | D664-A | 0.202 | | | Inflection Point | 60 mL |
| 6016 | D664-A | 0.292 | | 3.24 | Inflection Point | 60 mL |
| | GOST5985 | 0.1560 | | -1.04 | | |
| 6190 | | | | | | |
| | | | | | BEP (pH 11) only | Inflection Point only |
| | normality | OK | | | OK | OK |
| | , | ~- | | | | |
| | n outliers | 37 0 | | | 10 0 | 11 0 |
| | mean (n) | 0.1891 | | | 0.1598 | 0.2336 |
| | st.dev. (n) | 0.06788 | | | 0.05914 | 0.02855 |
| | R(calc.) | 0.00766 | | | 0.1656 | 0.0799 |
| | st.dev.(D664-A:17a, BEP (pH 11) 60mL) | 0.1901 | | | 0.02692 | 0.0799 |
| | | | | | | |
| | R(D664-A:17a, BEP (pH 11) 60mL) | 0.0888 | | | 0.0754 | |
| | compare st.dev.(D664-A:17a, Inflection - 60 mL) | 0.03666 | | | | 0.04359 |
| | R(D664-A:17a, Inflection - 60 mL) | 0.03666 | | | | 0.1221 |
| | NUDOUT-A. IT a, ITHIECTION - OU HIL) | 0.1020 | | | | V. 122 I |
| | | | | | | |

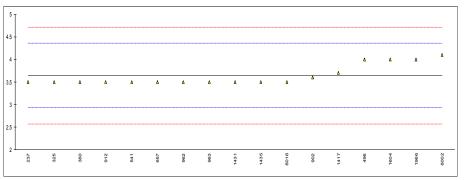


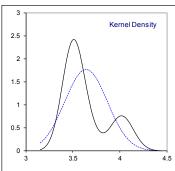


Determination of Color ASTM on sample #18077;

| lab | method | value | mark | z(targ) | calc. value*) | remarks |
|------|-------------------|-------------|------|---------|---------------|--------------------------------------|
| 178 | | | | | | |
| 179 | D1500 | L3.5 | | | 3.25 | |
| 225 | | | | | | |
| 237 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 325 | D6045 | 3.5 | | -0.40 | 3.5 | |
| 331 | D0070 | | | -0.40 | J.J | |
| 349 | D6045 | L4,0 | | | 3.75 | |
| 360 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 432 | D1500 D1500 | | | | | nessible false negative test requit? |
| | D1500 | L0,5 | | | 0.25 R(0.01) | possible false negative test result? |
| 451 | D4500 | | | | 2.25 | |
| 494 | D1500 | L3,5 | | 4.00 | 3.25 | |
| 496 | D1500 | 4.0 | | 1.00 | 4.0 | |
| 541 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 603 | D1500 | L4.0 | | | 3.75 | |
| 614 | D1500 | <4.0 | | | 3.75 | |
| 633 | D1500 | L3.5 | | | 3.25 | |
| 657 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 663 | D1500 | L4.0 | | | 3.75 | |
| 840 | D1500 | L4.0 | | | 3.75 | |
| 862 | D1500 | L0.5 | | | 0.25 R(0.01) | possible false negative test result? |
| 902 | D1500 | 3.6 | | -0.12 | 3.6 | |
| 912 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 962 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 963 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 974 | D1500 | L4.0 | | | 3.75 | |
| 1017 | | | | | | |
| 1023 | | | | | | |
| 1026 | D1500 | L4.0 | | | 3.75 | |
| 1059 | D1500 | L4,0 | | | 3.75 | |
| 1146 | B 1000 | | | | | |
| 1327 | D1500 | <3.5 | | | 3.25 | |
| 1417 | D6045 | 3.7 | | 0.16 | 3.7 | |
| 1431 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 1435 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 1456 | | 5.5 L4.0 | | -0.40 | 3.75 | |
| | D1500 | | | | | |
| 1604 | D1500 | 4.0 | | 1.00 | 4.0 | |
| 1875 | | | | | | |
| 1943 | D4500 | 4.0 | | 4.00 | 4.0 | |
| 1966 | D1500 | 4.0 | | 1.00 | 4.0 | |
| 6002 | D1500 | 4.1 | | 1.28 | 4.1 | |
| 6016 | D1500 | 3.5 | | -0.40 | 3.5 | |
| 6030 | | | | | | |
| 6190 | | | | | | |
| | | | | | | |
| | normality | suspect | | | OK | |
| | n | 17 | | | 30 | |
| | outliers | 0 | | | 2 | |
| | mean (n) | 3.64 | | | 3.62 | |
| | st.dev. (n) | 0.227 | | | 0.230 | |
| | R(calc.) | 0.63 | | | 0.64 | |
| | st.dev.(D1500:12) | 0.357 | | | 0.357 | |
| | R(D1500:12) | 1 | | | 1 | |
| | * | | | | | |

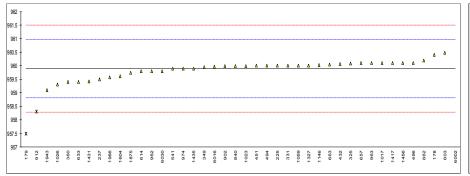
^{*)} In the calculation of the mean, standard deviation and the reproducibility in this column, a reported value of 'L y' is changed tot y-0.25 (for example L4.0 into 3.75).

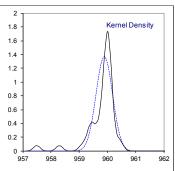




Determination of Density at 15°C on sample #18077; results in kg/m³

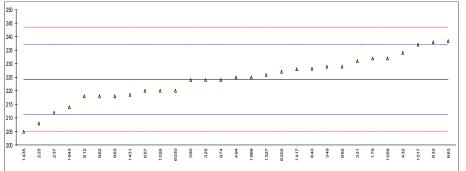
| 178 D1298 96.4 0.94 179 D1298 957.5 C,R(0.01) -4.47 179 D1298 959.5 0.10 179 D4052 960.0 0.36 179 D4052 960.0 0.36 179 D4052 960.0 0.39 179 D4052 960.0 0.31 170 D4052 960.0 0.38 170 D4052 960.0 0.39 170 D4052 960.0 0.38 170 D4052 960.0 0.39 170 D405 | lab | method | value | mark | z(targ) | remarks |
|--|------|---------------|--------|-----------|---------|------------------------------------|
| 179 D1298 95.7.5 C,R(0.01) - 4.47 first reported: 863.4 225 D4052 99.5 0.0 19 237 D4052 99.5 0.0 0.36 231 ISO12185 960.0 0.19 349 D4052 95.9 5 0.10 360 ISO12185 99.4 -0.93 442 D4052 960.0 0.19 444 D4052 960.0 0.19 449 D4052 960.0 0.19 449 D4052 960.0 0.19 449 D4052 960.1 0.40 541 D4052 960.1 0.40 541 D4052 99.9 0.01 603 D4052 99.9 0.01 614 D4052 99.8 -0.18 633 D1298 95.9 1 0.01 636 D4052 960.10 0.38 637 D4052 960.10 0.38 638 D4052 960.2 0.57 902 D4052 959.9 0.17 902 D4052 959.9 0.17 902 D4052 959.9 0.17 902 D4052 959.9 0.17 903 D4052 959.9 0.17 904 D4052 959.9 0.17 905 D4052 959.9 0.17 906 D4052 959.9 0.17 907 D4052 959.9 0.17 908 D4052 959.9 0.17 909 D4052 959.9 0.17 909 D4052 959.9 0.17 901 D4052 959.9 0.17 902 D4052 959.9 0.17 903 D4052 959.9 0.17 904 D4052 959.9 0.17 905 D4052 959.9 0.17 906 D4052 959.9 0.17 907 D4052 959.9 0.17 908 D4052 959.9 0.17 909 D4052 959.9 0.1 | | | | | | |
| 225 D4052 960.0 0.19 237 D4052 959.5 0.74 325 D4052 960.09 0.36 331 IS012185 960.0 0.19 339 D4052 959.5 0.10 339 D4052 959.5 0.10 330 IS012185 950.4 0.93 432 D4052 960.0 0.19 434 D4052 960.0 0.19 436 D4052 960.0 0.19 437 D4052 960.0 0.19 438 D4052 960.1 0.40 439 D4052 960.1 0.40 440 D4052 960.1 0.40 451 D4052 960.47 1.07 461 D4052 960.1 0.38 463 D4052 960.10 0.38 464 D4052 960.10 0.38 465 D4052 960.10 0.38 467 D4052 960.10 0.38 468 D4052 960.10 0.38 469 D4052 960.0 0.17 460 D4052 960.1 0.38 461 D4052 960.1 0.38 462 D4052 960.2 0.57 462 D4052 960.1 0.38 463 D4052 960.1 0.38 463 D4052 960.1 0.38 464 D4052 960.1 0.38 465 D4052 960.1 0.38 466 D4052 960.1 0.38 467 D4052 960.1 0.38 468 D4052 960.1 0.38 469 D4052 960.1 0.38 469 D4052 960.1 0.38 461 D4052 960.0 0.19 466 D4052 960.1 0.38 467 D4052 960.1 0.38 468 D4052 960.1 0.38 469 D4052 960.1 0.38 460 D4052 960.1 0.38 461 D4052 960.1 0.38 461 D4052 960.0 0.19 466 D4052 960.1 0.38 467 D4052 960.1 0.38 468 D4052 960.1 0.38 469 D4052 960.1 0.38 460 D4052 960.0 0.19 460 D4052 960.0 0.19 460 D4052 960.1 0.38 460 D4052 960.1 0.38 460 D4052 960.1 0.38 460 D4052 960.0 0.19 460 D4052 960.1 0.38 460 D4052 960.0 0.19 460 D405 | | | | C,R(0.01) | | first reported: 863.4 |
| 237 D4052 959.5 -0.74 325 D4052 960.09 0.36 331 ISO12185 960.0 0.19 349 D4052 959.95 0.10 360 ISO12185 959.4 -0.93 432 D4052 960.06 0.31 431 D4052 960.0 0.19 494 D4052 960.0 0.19 494 D4052 960.1 0.40 541 D4052 959.9 0.01 633 D4052 959.9 0.01 644 D4052 959.8 -0.18 633 D1298 959.4 -0.91 657 D4052 960.1 0.38 658 D4052 960.1 0.38 658 D4052 960.1 0.38 659 D4052 960.1 0.38 661 D4052 959.9 0.17 662 D4052 959.9 0.17 663 D4052 959.9 0.17 664 D4052 959.9 0.17 665 D4052 960.1 0.38 667 D4052 960.1 0.38 668 D4052 960.1 0.38 669 D4052 959.9 0.17 660 D4052 959.9 0.17 661 D4052 960.1 0.38 662 D4052 960.1 0.38 663 D4052 960.1 0.38 663 D4052 960.1 0.38 664 D4052 969.9 0.17 665 D4052 960.1 0.38 666 D4052 969.9 0.17 666 D4052 969.9 0.17 667 D4052 960.1 0.38 668 D4052 969.9 0.17 668 D4052 969.9 0.17 669 D4052 969.9 0.17 669 D4052 969.9 0.17 660 D4052 969.9 0 | | D4052 | | , , , | | • |
| 325 D4052 960.09 0.36 331 ISO12185 960.0 0.19 349 D4052 959.95 0.10 349 D4052 960.06 0.31 451 D4052 960.06 0.31 451 D4052 960.0 0.19 496 D4052 960.1 0.40 4054 D4052 960.1 0.40 4054 D4052 960.1 0.40 4054 D4052 960.1 0.40 4054 D4052 960.1 0.38 633 D1298 959.4 0.91 0.38 663 D4052 960.10 0.38 663 D4052 960.05 0.29 0.17 0.4052 960.2 0.57 0.17 0.4052 960.2 0.57 0.17 0.4052 960.1 0.38 0.18 | | | | | | |
| 331 ISO12185 980.0 0.19 349 D4052 959.95 0.10 360 ISO12185 959.4 -0.93 432 D4052 960.06 0.31 431 D4052 960.0 0.19 4494 D4052 960.0 0.19 4494 D4052 960.0 0.19 4494 D4052 959.9 0.01 541 D4052 959.9 0.01 603 D4052 959.9 0.01 614 D4052 959.4 -0.98 633 D1288 959.41 -0.91 667 D4052 960.05 0.29 840 D4052 959.9 0.17 8682 D4052 960.05 0.29 840 D4052 959.9 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 959.9 0.17 912 D1298 958.3 R(0.01) -2.98 963 D4052 959.9 0.17 1017 D4052 960.1 0.38 1023 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.01 1046 D4052 959.9 0.01 1059 ISO12185 960.0 0.19 146 D4052 950.0 0.25 1417 D4052 960.1 0.38 1431 D4052 959.9 0.01 1446 D4052 959.9 0.01 1447 D4052 950.1 0.38 14431 D4052 959.9 0.01 1446 D4052 959.9 0.01 1447 D4052 950.1 0.38 14431 D4052 959.9 0.01 1446 D4052 959.9 0.01 1447 D4052 950.1 0.38 1451 D4052 959.9 0.01 1460 D4052 959.9 0.01 147 D4052 950.1 0.38 1487 D4052 959.9 0.01 149052 959.1 0.38 1491 D4052 959.9 0.01 149062 959.9 0.01 149062 959.9 | 325 | D4052 | | | | |
| 349 D4052 959.94 - 0.93 360 ISO12185 959.4 - 0.93 432 D4052 960.06 0.31 4451 D4052 960.0 0.19 4464 D4052 960.0 0.19 4466 D4052 960.1 0.40 541 D4052 960.1 0.40 541 D4052 960.4 1.07 643 D4052 960.4 1.07 644 D4052 959.8 - 0.18 633 D1298 959.41 - 0.91 6657 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 950.9 0.17 862 D4052 950.9 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.9 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.9 0.17 912 D1298 959.9 0.17 912 D1298 959.9 0.17 913 D4052 959.9 0.17 107 D4052 959.9 0.17 107 D4052 959.9 0.17 108 D4052 959.9 0.17 109 D4052 959.9 0.17 1017 D4052 960.1 0.38 1023 D4052 959.3 -1.11 1059 ISO12185 960.0 C 0.19 1146 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1023 D4052 959.9 0.01 1446 D4052 959.4 0.89 1435 D4052 959.9 0.01 1447 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1475 ISO12185 959.75 C -0.27 1476 D4052 959.9 0.01 1447 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1986 D1298 959.75 C -0.27 1996 D1298 959.75 C -0.27 1997 D1298 959.75 C -0.27 1996 D1298 D12 | | | | | | |
| 360 ISO12185 95.4 -0.93 432 D4052 960.06 0.31 451 D4052 960.0 0.19 494 D4052 960.0 0.19 494 D4052 960.0 0.19 541 D4052 959.90 0.01 541 D4052 959.90 0.01 603 D4052 959.90 0.01 614 D4052 959.8 -0.18 633 D1288 959.41 -0.91 657 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 960.2 0.57 902 D4052 959.99 0.17 912 D1298 958.3 R(0.01) 2.98 963 D4052 950.1 0.38 974 D4052 959.9 0.01 1017 D4052 950.1 0.38 1023 D4052 950.1 0.38 1023 D4052 950.1 0.38 1023 D4052 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10465 959.9 0.17 10466 D4052 959.9 0.17 1059 ISO12185 960.0 0.19 1146 D4052 959.9 0.17 1417 D4052 960.1 0.38 1431 D4052 959.9 0.01 1447 D4052 960.1 0.38 1431 D4052 959.9 0.01 1447 D4052 960.1 0.38 1443 D4052 959.9 0.01 1447 D4052 960.1 0.38 1443 D4052 959.9 0.01 1446 D4052 959.9 0.01 1447 D4052 960.1 0.38 1604 D1298 959.61 C 0.53 1875 ISO12185 960.0 C 0.19 1485 D4052 959.9 0.01 1496 D4052 959.9 0.01 1497 D4052 950.1 0.38 1604 D1298 959.61 C 0.53 1875 ISO12185 959.9 0.01 1496 D1298 959.61 C 0.53 1876 ISO12185 959.9 0.01 1496 D1298 959.61 C 0.53 1877 ISO12185 959.9 0.01 1496 D4052 959.9 0.01 1497 D4052 950.1 0.38 1604 D1298 959.61 C 0.53 1876 ISO12185 959.9 0.01 1496 D1298 959.61 C 0.57 1943 ISO3675 95.6 R(0.01) 46.86 016 D4052 959.9 0.01 1007 D707 D707 D707 D707 D707 D707 D707 | | | | | | |
| 432 D4052 960.06 0.31 451 D4052 960.0 0.19 494 D4052 960.0 0.19 494 D4052 960.11 0.40 541 D4052 959.90 0.01 603 D4052 960.47 1.07 614 D4052 959.8 -0.18 633 D1298 959.41 -0.91 667 D4052 960.10 0.38 663 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 959.99 0.17 912 D1298 959.3 R(0.01) -2.98 962 D4052 959.9 0.17 912 D1298 959.8 -0.18 963 D4052 960.1 0.38 963 D4052 959.9 0.17 1017 D4052 959.9 0.01 1017 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1027 D4052 959.9 0.17 1028 D4052 959.9 0.17 1029 B4052 959.9 0.17 1029 D4052 959.9 0.17 1026 D4052 959.9 0.17 1027 D4052 959.9 0.17 1028 D4052 959.9 0.17 1029 D4052 959.9 0.17 1020 D4052 959.9 0 | | | | | | |
| 451 D4052 960 0 0.19 494 D4052 960.0 0.19 496 D4052 960.1 0.40 541 D4052 959.90 0.01 603 D4052 959.90 0.01 614 D4052 959.8 -0.18 633 D1298 959.41 -0.91 667 D4052 960.0 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 960.9 0.17 862 D4052 960.9 0.17 862 D4052 959.99 0.17 862 D4052 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.99 0.17 912 D1298 959.8 -0.18 963 D4052 960.1 0.38 963 D4052 960.1 0.38 974 D4052 960.1 0.38 1023 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1027 D4052 960.1 0.38 1023 D4052 959.9 0.17 10465 960.0 0.19 1141 D4052 960.1 0.38 1043 D4052 959.9 0.01 1447 D4052 960.1 0.38 1431 D4052 959.9 0.01 1447 D4052 959.9 0.01 1447 D4052 960.1 0.38 1860 D4052 959.9 0.01 1471 D4052 959.9 0.01 1472 D4052 959.9 0.01 1473 D4052 959.9 0.01 1474 D4052 959.9 0.01 1475 D4052 959.9 0.01 1476 D4052 959.9 0.01 1477 D4052 960.1 0.38 1876 IS012185 960.0 C 0.19 1478 D4052 959.9 0.01 1479 D4052 959.9 0.01 1479 D4052 959.9 0.01 1479 D4052 959.9 0.01 1479 D4052 959.9 0.01 1470 D4052 959.9 0.01 1471 D4052 959.9 0.01 1471 D4052 959.9 0.01 1472 D4052 959.9 0.01 1473 D4052 959.9 0.01 1475 D4052 959.9 0.01 1476 D4052 959.9 0.01 1477 D4052 959.9 0.01 1478 D4052 959.9 0.01 1479 D4052 959.9 0.01 1470 D4052 959.9 0.01 1471 D4052 959.9 0.01 1472 D4052 959.9 0.01 1475 D4052 959.9 0.01 | | | | | | |
| 494 D4052 960.0 0.19 496 D4052 960.11 0.40 541 D4052 959.90 0.01 603 D4052 960.47 1.07 614 D4052 959.8 -0.18 633 D1296 959.41 -0.91 667 D4052 960.05 0.29 840 D4052 960.05 0.29 840 D4052 959.9 0.17 862 D4052 959.9 0.17 912 D1296 958.3 R(0.01) 2.98 962 D4052 959.9 9.0.17 912 D1296 958.3 R(0.01) 2.98 962 D4052 959.9 9.0.17 912 D1296 959.9 9.0.17 1017 D4052 960.1 0.38 1023 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.1 0.38 1431 D4052 959.9 0.01 1456 D4052 960.1 0.38 1431 D4052 959.9 0.01 1456 | | | | | | |
| 496 D4052 950.11 0.40 541 D4052 959.90 0.01 603 D4052 950.47 1.07 614 D4052 959.8 -0.18 633 D1298 959.41 -0.91 667 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 960.2 0.57 902 D4052 959.99 0.17 912 D1298 988.3 R(0.01) -2.98 962 D4052 959.99 0.01 912 D1298 988.3 R(0.01) -2.98 962 D4052 959.9 0.01 1017 D4052 960.1 0.38 974 D4052 959.9 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.25 1327 D4052 960.1 0.38 1417 D4052 960.1 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | | |
| 541 D4052 959.90 0.01 603 D4052 960.47 1.07 614 D4052 959.8 -0.18 633 D1298 959.41 -0.91 667 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 960.2 0.57 902 D4052 969.9 0.17 962 D4052 959.9 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 0.18 963 D4052 959.8 0.18 963 D4052 959.9 0.01 1017 D4052 959.9 0.01 1027 D4052 959.9 0.17 1028 D4052 959.9 0.17 1029 D4052 959.3 -1.11 1059 IS012185 960.0 0.19 1446 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 960.1 0.38 1435 D4052 960.1 0.38 1436 D4052 960.1 | | | | | | |
| 603 D4052 960.47 1.07 614 D4052 959.8 -0.18 633 D1298 959.41 -0.91 667 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 959.99 0.17 862 D4052 959.99 0.17 862 D4052 959.99 0.17 862 D4052 959.99 0.17 863 D4052 959.99 0.17 864 D4052 959.8 3 R(0.01) -2.98 865 D4052 960.1 0.38 866 D4052 960.1 0.38 867 D4052 960.1 0.38 867 D4052 960.1 0.38 868 D4052 960.1 0.38 869 D4052 960.1 0.38 869 D4052 960.1 0.38 869 D4052 959.99 0.17 860 D4052 959.99 0.17 861 D4052 960.0 0.19 862 D4052 959.99 0.17 863 D4052 959.99 0.17 864 D4052 959.91 0.19 865 D4052 960.0 0.19 866 D4052 960.0 0.19 866 D4052 960.1 0.38 867 D4052 960.1 0.38 868 D4052 960.1 0.38 868 D4052 960.1 0.38 869 D4052 960.1 0.38 860 D4052 960.0 0.19 86 | | | | | | |
| 614 D4052 959.8 -0.18 633 D1298 959.41 -0.91 6657 D4052 960.01 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 960.2 0.57 902 D4052 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.9 0.17 912 D1298 958.3 R(0.01) -2.98 963 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.3 -1.11 1059 ISC12185 960.0 0.19 1146 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 960.0 C 0.19 1445 D4052 960.0 C 0.19 1445 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1445 D4052 959.9 0.01 1456 D4052 950.0 0.00 1456 D4052 950.0 0.00 1456 D4052 950.0 | | | | | | |
| 633 D1288 959.41 -0.91 657 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 959.99 0.17 912 D1288 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 960.1 0.38 963 D4052 960.1 0.38 964 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1030 D4052 960.1 0.38 1023 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.1 0.38 1431 D4052 960.1 0.38 1435 D4052 960.1 0.38 1436 D4052 959.9 0.01 1456 D4052 959.9 0.01 1456 D4052 959.9 0.01 1456 D4052 959.9 0.01 1456 D4052 959.1 -1.49 1966 D1298 959.58 -0.59 1875 ISO12185 959.75 C -0.27 1876 D4052 959.9 10.1 1966 D1298 959.58 R(0.01) 46.86 190 | | | | | | |
| 657 D4052 960.10 0.38 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 950.92 0.57 902 D4052 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 959.9 0.01 1017 D4052 959.9 0.01 1017 D4052 950.1 0.38 1023 D4052 959.9 0.01 1017 D4052 960.1 0.38 1023 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.03 0.25 1327 D4052 960.01 0.38 1431 D4052 960.0 C 0.19 1447 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 959.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 16002 ISO3675 985 R(0.01) 46.86 1600 D4052 959.97 1000 S03675 985 -0.18 1000 GOST3900 959.8 -0.18 1000 GOST3900 959.8 -0.18 1000 St.dev. (n) 0.291 | | | | | | |
| 663 D4052 960.05 0.29 840 D4052 959.99 0.17 862 D4052 960.2 0.57 902 D4052 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 960.1 0.38 974 D4052 960.1 0.38 1023 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.9 0.17 1046 D4052 960.0 0.19 1146 D4052 960.0 C 0.19 1147 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 959.61 C -0.53 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1943 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 1966 D1298 959.58 -0.18 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| 840 D4052 959.99 0.17 862 D4052 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 959.9 0.01 1017 D4052 959.9 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1146 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 959.4 0.89 1435 D4052 959.4 0.89 1435 D4052 959.4 10.38 1431 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 959.4 0.89 1435 D4052 960.1 0.38 1604 D1298 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6010 Tormality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| 862 D4052 960.2 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 960.1 0.38 974 D4052 960.1 0.38 1023 D4052 960.1 0.38 1023 D4052 959.9 0.17 1016 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1141 D4052 960.1 0.38 1431 D4052 960.1 0.38 1436 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6090 st.dev. (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| 902 D4052 959.99 0.17 912 D1298 958.3 R(0.01) -2.98 962 D4052 959.8 -0.18 963 D4052 960.1 0.38 974 D4052 959.9 0.01 1017 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1147 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 959.9 0.01 1435 D4052 959.9 0.01 1436 D4052 959.9 1.01 1437 D4052 959.9 1.01 1438 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.1 -1.49 1966 D1298 959.5 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.59 6002 ISO3675 985 R(0.01) 46.86 6019 | | | | | | |
| 962 D4052 959.8 -0.18 963 D4052 960.1 0.38 974 D4052 959.9 0.01 1017 D4052 959.9 0.07 1017 D4052 959.99 0.17 1026 D4052 959.99 0.17 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1417 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 959.9 0.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | | | | | | |
| 962 D4052 959.8 -0.18 963 D4052 960.1 0.38 974 D4052 959.9 0.01 1017 D4052 959.9 0.07 1017 D4052 959.99 0.17 1026 D4052 959.99 0.17 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1417 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 959.9 0.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.9 1.01 1456 D4052 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 912 | D1298 | 958.3 | R(0.01) | -2.98 | |
| 963 D4052 960.1 0.38 974 D4052 959.9 0.01 1017 D4052 959.9 0.17 1026 D4052 959.9 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.7 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.9 0.14 6030 GOST3900 959.8 -0.18 6190 | 962 | D4052 | 959.8 | ` , | -0.18 | |
| 1017 D4052 960.1 0.38 1023 D4052 959.99 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.0 C 0.19 1147 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1460 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 963 | D4052 | 960.1 | | | |
| 1023 D4052 959.99 0.17 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.03 0.25 1327 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 974 | D4052 | 959.9 | | 0.01 | |
| 1026 D4052 959.3 -1.11 1059 ISO12185 960.0 0.19 1146 D4052 960.03 0.25 1327 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 1017 | D4052 | 960.1 | | 0.38 | |
| 1059 ISO12185 960.0 0.19 1146 D4052 960.03 0.25 1327 D4052 960.0 C 0.19 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 1875 ISO12185 959.75 C -0.27 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 1023 | D4052 | 959.99 | | 0.17 | |
| 1146 D4052 960.03 0.25 1327 D4052 960.0 C 0.19 reported: 0.9600 kg/m³ 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 1026 | D4052 | 959.3 | | -1.11 | |
| 1327 D4052 960.0 C 0.19 reported: 0.9600 kg/m³ 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 0K normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 1059 | ISO12185 | 960.0 | | 0.19 | |
| 1417 D4052 960.1 0.38 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 1146 | D4052 | 960.03 | | 0.25 | |
| 1431 D4052 959.42 -0.89 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 1327 | D4052 | 960.0 | С | 0.19 | reported: 0.9600 kg/m ³ |
| 1435 D4052 959.9 0.01 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | D4052 | 960.1 | | | |
| 1456 D4052 960.1 0.38 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 1431 | D4052 | 959.42 | | -0.89 | |
| 1604 D1298 959.61 C -0.53 reported: 0.9561 kg/m³ 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | 1435 | D4052 | 959.9 | | 0.01 | |
| 1875 ISO12185 959.75 C -0.27 first reported: 956.95 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 1456 | D4052 | 960.1 | | | |
| 1943 ISO3675 959.1 -1.49 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | D1298 | 959.61 | | | reported: 0.9561 kg/m ³ |
| 1966 D1298 959.58 -0.59 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 1875 | ISO12185 | 959.75 | С | -0.27 | first reported: 956.95 |
| 6002 ISO3675 985 R(0.01) 46.86 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 | | | | | | |
| 6016 D4052 959.97 0.14 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| 6030 GOST3900 959.8 -0.18 6190 normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | | R(0.01) | | |
| normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| normality OK n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | GOST3900 | 959.8 | | -0.18 | |
| n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | 6190 | | | | | |
| n 39 outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | 014 | | | |
| outliers 3 mean (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| mean (n) 959.90 st.dev. (n) 0.291 | | | | | | |
| st.dev. (n) 0.291 | | | | | | |
| | | ` , | | | | |
| 11/00/01 | | ` , | | | | |
| R(calc.) 0.82 | | | | | | |
| st.dev.(D1298:12b) 0.536 R(D1298:12b) 1.5 | | ` , | | | | |
| R(D1298:12b) 1.5 | | 11(11230.120) | 1.5 | | | |

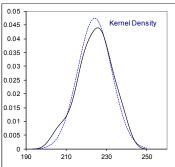




Determination of Flash Point COC on sample #18077; results in °C

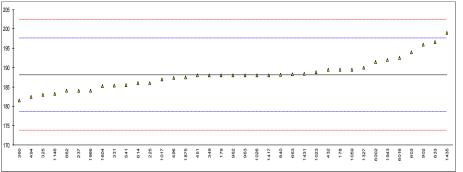
| lab | method | value | mark | z(targ) | remarks |
|------|------------------|--------|------|---------|---------|
| 178 | | | | | |
| 179 | D92 | 232 | | 1.21 | |
| 225 | D92 | 208.0 | | -2.53 | |
| 237 | D92 | 212 | | -1.90 | |
| 325 | | 224 | | -0.04 | |
| | D92 | | | | |
| 331 | D92 | 231.0 | | 1.05 | |
| 349 | D92 | 229 | | 0.74 | |
| 360 | D92 | 224 | | -0.04 | |
| 432 | D92 | 234 | | 1.52 | |
| 451 | | | | | |
| 494 | D92 | 225 | | 0.12 | |
| 496 | | | | | |
| 541 | | | | | |
| 603 | | | | | |
| 614 | | | | | |
| 633 | D92 | 238 | | 2.14 | |
| 657 | D92 | 220 | | -0.66 | |
| 663 | D92 | 238.3 | | 2.19 | |
| | | | | | |
| 840 | D92 | 228.1 | | 0.60 | |
| 862 | D92 | 229 | | 0.74 | |
| 902 | | | | | |
| 912 | D92 | 218 | | -0.97 | |
| 962 | D92 | 218 | | -0.97 | |
| 963 | D92 | 218 | | -0.97 | |
| 974 | D92 | 224 | | -0.04 | |
| 1017 | D92 | 237 | | 1.99 | |
| 1023 | | | | | |
| 1026 | D92 | 220 | | -0.66 | |
| 1059 | ISO2592 | 232 | | 1.21 | |
| 1146 | | | | | |
| 1327 | D92 | 226 | | 0.27 | |
| 1417 | D92 | 228 | | 0.59 | |
| 1431 | D92 | 218.5 | | -0.89 | |
| 1435 | D92 | 205.0 | | -2.99 | |
| 1456 | D92 | | | -2.55 | |
| | | | | | |
| 1604 | | | | | |
| 1875 | 1000500 | | | 4.50 | |
| 1943 | ISO2592 | 214 | | -1.59 | |
| 1966 | D92 | 225 | | 0.12 | |
| 6002 | ISO2592 | 227 | | 0.43 | |
| 6016 | | | | | |
| 6030 | GOST4333 | 220 | | -0.66 | |
| 6190 | | | | | |
| | | | | | |
| | normality | OK | | | |
| | n | 29 | | | |
| | outliers | 0 | | | |
| | mean (n) | 224.24 | | | |
| | st.dev. (n) | 8.430 | | | |
| | R(calc.) | 23.60 | | | |
| | st.dev.(D92:16b) | 6.429 | | | |
| | | | | | |
| | R(D92:16b) | 18 | | | |
| | | | | | |

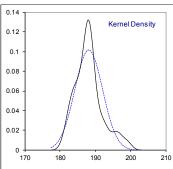




Determination of Flash Point PMcc on sample #18077; results in °C

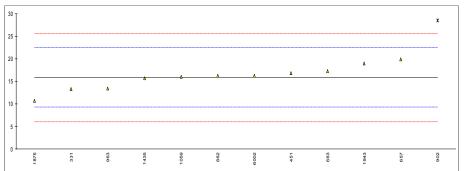
| lab | method | value | mark | z(targ) | remar | ks | | | |
|--------------|------------------------------------|----------------|------------|---------------------|-------|----------------|---------------|--------------------------|----------|
| 178 | D93-A | 189.5 | | 0.28 | | | | | |
| 179 | D93-A | 188.0 | | -0.03 | | | | | |
| 225 | D93-B | 186.0 | | -0.45 | | | | | |
| 237 | D93-B | 184.0 | | -0.87 | | | | | |
| 325 | D93-A | 183 | | -1.08 | | | | | |
| 331 | D93-B | 185.3 | | -0.60 | | | | | |
| 349 | D93-A | 188 | | -0.03 | | | | | |
| 360 | D93-B | 181.5 | | -1.39 | | | | | |
| 432 | D93-A | 189.5 | | 0.28 | | | | | |
| 451 | D93-A | 188 | | -0.03 | | | | | |
| 494 | D93-B | 182.5 | | -1.18 | | | | | |
| 496 | D93-A | 187.3 | | -0.18 | | | | | |
| 541 | D93-A | 185.50 | | -0.56 | | | | | |
| 603 | D93-A | 194 | | 1.23 | | | | | |
| 614 | D93-A | 186 | | -0.45 | | | | | |
| 633 | D93-A | 196.58 | | 1.77 | | | | | |
| 657 | | | | | | | | | |
| 663 | D93-A | 188.30 | | 0.03 | | | | | |
| 840 | D93-B | 188.1 | | -0.01 | | | | | |
| 862 | D93-A | 184 | | -0.87 | | | | | |
| 902 | D93-A | 196.0 | | 1.64 | | | | | |
| 912 | | | | | | | | | |
| 962 | D93-A | 188 | | -0.03 | | | | | |
| 963 | D93-A | 188 | | -0.03 | | | | | |
| 974 | D00 4 | 407.0 | | | | | | | |
| 1017 | D93-A | 187.0 | | -0.24 | | | | | |
| 1023 1026 | D93-A ISO2719-A | 188.8 | | 0.14 -0.03 | | | | | |
| 1020 | ISO2719-A ISO2719-A | 188 189.5 | | 0.03 | | | | | |
| 1146 | D93-A | 183.2 | | -1.04 | | | | | |
| 1327 | D93-A | 190.0 | | 0.39 | | | | | |
| 1417 | D93-A | 188 | | -0.03 | | | | | |
| 1431 | D93-A | 188.4 | | 0.05 | | | | | |
| 1435 | D93-A | 199.0 | | 2.27 | | | | | |
| 1456 | 2007. | | | | | | | | |
| 1604 | D93 | 185.2 | | -0.62 | | | | | |
| 1875 | ISO2719-B | 187.5 | | -0.14 | | | | | |
| 1943 | ISO2719-A | 192 | | 0.81 | | | | | |
| 1966 | D93-A | 184 | | -0.87 | | | | | |
| 6002 | D93-A | 191.5 | | 0.70 | | | | | |
| 6016 | D93-A | 192.5 | | 0.91 | | | | | |
| 6030 | | | | | | | | | |
| 6190 | | | | | | | | | |
| | | | | | | | O2719 meth. A | Only D93/ISO2719 meth. E | <u>3</u> |
| | normality | OK | | | | OK | | OK | |
| | n | 37 | | | | 29 | | 7 | |
| | outliers | 0 | | | | 0 | | 0 | |
| | mean (n) | 188.15 | | | | 189.02 | | 184.99 | |
| | st.dev. (n) | 3.921 | | | | 3.856 | | 2.465 | |
| | R(calc.) | 10.98 | | | | 10.80 | | 6.90 | |
| | st.dev.(D93-A:16a) R(D93-A:16a) | 4.771 13.36 | Comp. R(D9 | 3-B-16a) - | - 10 | 4.793 13.42 | | 3.571 10 | |
| | N(D95-A. 10a) | 13.30 | Comp. R(DS | -о-ы. тоа) - | - 10 | 10.42 | | 10 | |

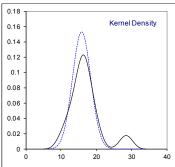




Determination of Insoluble Color Bodies, membrane patch colorimetry on sample #18077;

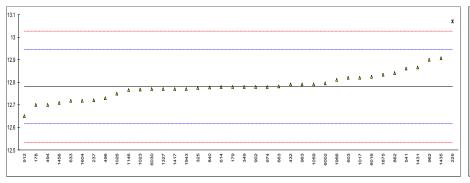
| lab | method | value | mark | z(targ) | remarks |
|------|-------------------|--------|---------|---------|---------|
| 178 | | | | | |
| 179 | | | | | |
| 225 | | | | | |
| 237 | | | | | |
| 325 | | | | | |
| 331 | D7843 | | | | |
| | D7643 | 13.3 | | -0.78 | |
| 349 | | | | | |
| 360 | | | | | |
| 432 | 5-0.40 | | | | |
| 451 | D7843 | 16.8 | | 0.29 | |
| 494 | | | | | |
| 496 | | | | | |
| 541 | | | | | |
| 603 | | | | | |
| 614 | | | | | |
| 633 | | | | | |
| 657 | D7843 | 19.83 | | 1.21 | |
| 663 | D7843 | 17.3 | | 0.44 | |
| 840 | | | | | |
| 862 | D7843 | 16.2 | | 0.10 | |
| 902 | D7843 | 28.5 | G(0.05) | 3.86 | |
| 912 | 2.5.5 | | 3(0.00) | | |
| 962 | | | | | |
| 963 | D7843 | 13.4 | | -0.75 | |
| 974 | 27010 | | | | |
| 1017 | | | | | |
| 1023 | | | | | |
| 1025 | | | | | |
| 1059 | D7843 | 16 | | 0.04 | |
| 1146 | D7643 | | | | |
| | | | | | |
| 1327 | | | | | |
| 1417 | | | | | |
| 1431 | D7040 | 45.7 | | | |
| 1435 | D7843 | 15.7 | | -0.05 | |
| 1456 | | | | | |
| 1604 | | | | | |
| 1875 | D7843 | 10.7 | | -1.57 | |
| 1943 | D7843 | 18.958 | | 0.95 | |
| 1966 | | | | | |
| 6002 | D7843 | 16.24 | | 0.12 | |
| 6016 | | | | | |
| 6030 | | | | | |
| 6190 | | | | | |
| | | | | | |
| | normality | OK | | | |
| | n | 11 | | | |
| | outliers | 1 | | | |
| | mean (n) | 15.86 | | | |
| | st.dev. (n) | 2.605 | | | |
| | R(calc.) | 7.29 | | | |
| | st.dev.(D7843:16) | 3.278 | | | |
| | R(D7843:16) | 9.18 | | | |
| | , | | | | |

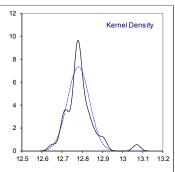




Determination of Kinematic Viscosity at 40°C on sample #18077; results in mm²/s

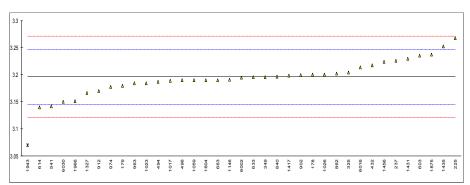
| lab | method | value | mark | z(targ) | remarks |
|------|-----------------------|-------------|---------|---------|---|
| 178 | D445 | 12.7 | | -0.98 | |
| 179 | D445 | 12.78 | | -0.01 | |
| 225 | D445 | 13.07 | R(0.01) | 3.52 | |
| 237 | D445 | 12.72 | , | -0.74 | |
| 325 | D445 | 12.774 | | -0.08 | |
| 331 | | | | | |
| 349 | D445 | 12.78 | С | -0.01 | first reported:12.58 |
| 360 | | | | | |
| 432 | D445 | 12.79 | | 0.11 | |
| 451 | | | | | |
| 494 | D445 | 12.701 | | -0.97 | |
| 496 | D445 | 12.729 | | -0.63 | |
| 541 | D7042 | 12.860 | | 0.97 | |
| 603 | D7042 | 12.820 | | 0.48 | |
| 614 | D445 | 12.78 | | -0.01 | |
| 633 | D7279 corr. to D445 | 12.717 | | -0.77 | |
| 657 | | | | | |
| 663 | D445 | 12.782 | | 0.02 | |
| 840 | D7042 | 12.776 | | -0.06 | |
| 862 | D445 | 12.84 | | 0.72 | |
| 902 | D445 | 12.78 | | -0.01 | |
| 912 | D445 | 12.65 | | -1.59 | |
| 962 | D445 | 12.90 | | 1.45 | |
| 963 | D445 | 12.79 | | 0.11 | |
| 974 | D445 | 12.78 | | -0.01 | |
| 1017 | D445 | 12.82 | | 0.48 | |
| 1023 | D445 | 12.769 | | -0.14 | |
| 1026 | D445 | 12.75 | | -0.37 | |
| 1059 | ISO3104 | 12.79 | | 0.11 | |
| 1146 | D445 | 12.766 | | -0.18 | |
| 1327 | D445 | 12.77 | | -0.13 | |
| 1417 | D445 | 12.77 | | -0.13 | |
| 1431 | D7042 | 12.866 | | 1.04 | |
| 1435 | D7042 | 12.906 | | 1.53 | |
| 1456 | D7042 | 12.71 | | -0.86 | |
| 1604 | D445 | 12.717 | | -0.77 | |
| 1875 | D7042 | 12.833 | | 0.64 | |
| 1943 | ISO3104 | 12.77 | | -0.13 | |
| 1966 | D445 | 12.81 | | 0.36 | |
| 6002 | ISO3104 | 12.794 | | 0.16 | |
| 6016 | D7042 | 12.825 | | 0.54 | |
| 6030 | GOST33 | 12.7697 | | -0.13 | |
| 6190 | | | | | |
| | normality | OK | | | |
| | normality n | 37 | | | |
| | outliers | 1 | | | |
| | mean (n) | 1 12.781 | | | |
| | st.dev. (n) | 0.0546 | | | |
| | R(calc.) | 0.0546 | | | |
| | st.dev.(iis, lit. 16) | 0.133 | | | |
| | R(iis, lit. 16) | 0.0022 | | | Compare R(D445:17) = 0.048, range 25 to125 mm ² /s |
| | (110, 111. 10) | 0.200 | | | 55ps. 5 13(5 1 15.11) 5.5 15, rango 25 to 125 mm 75 |

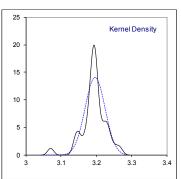




Determination of Kinematic Viscosity at 100°C on sample #18077; results in mm²/s

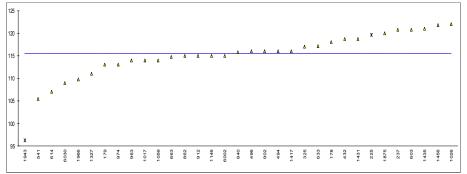
| lab | method | value | mark | z(targ) | remarks |
|--------------|------------------------|----------------|-----------|----------------|--|
| 178 | D445 | 3.20 | | 0.15 | |
| 179 | D445 | 3.180 | | -0.64 | |
| 225 | D445 | 3.267 | | 2.82 | |
| 237 | D445 | 3.226 | | 1.19 | |
| 325 | D445 | 3.204 | | 0.31 | |
| 331 | | | | | |
| 349 | D445 | 3.196 | | 0.00 | |
| 360 | | | | | |
| 432 | D445 | 3.217 | | 0.83 | |
| 451 | 2 | | | | |
| 494 | D445 | 3.1876 | | -0.34 | |
| 496 | D445 | 3.1896 | | -0.26 | |
| 541 | D7042 | 3.1417 | | -2.17 | |
| 603 | D7042 | 3.2357 | | 1.58 | |
| 614 | D445 | 3.14 | | -2.23 | |
| 633 | D445 | 3.1958 | | -0.01 | |
| 657 | D-170 | J. 1930 | | -0.01 | |
| 663 | D445 | 3.1903 | | -0.23 | |
| 840 | D7042 | 3.1963 | | 0.23 | |
| 862 | D445 | 3.1903 | | 0.01 | |
| 902 | D445 | 3.199 | | 0.23 | |
| 912 | | | | -1.04 | |
| 962 | D445 | 3.170 | | | |
| | D445 | 2 104 | | 0.49 | |
| 963 974 | D445 D445 | 3.184 3.178 | | -0.48 -0.72 | |
| | | | | | |
| 1017 1023 | D445 D445 | 3.189 | | -0.28 | |
| 1023 | D445 | 3.184 | | -0.48 0.15 | |
| 1059 | ISO3104 | 3.20 3.190 | | -0.24 | |
| | D445 | | | | |
| 1146 | | 3.1907 | | -0.22 | |
| 1327 | D445 | 3.166 | | -1.20 | |
| 1417 | D445 | 3.198 | | 0.07 1.32 | |
| 1431 | D7042 | 3.2292 | | | |
| 1435 | D7042 | 3.2527 | | 2.25 | |
| 1456 | D7042 | 3.224 | | 1.11 | |
| 1604 | D445 | 3.190 | | -0.24 | |
| 1875 | D7042 | 3.237 | C D(0.04) | 1.63 | first reported: 2.44 |
| 1943 | ISO3104 | 3.07 | C,R(0.01) | -5.02 | first reported: 3.11 |
| 1966 | D445 | 3.151 | | -1.80 | |
| 6002 | ISO3104 | 3.195 | | -0.04 | |
| 6016 | D7042 | 3.2139 | | 0.71 | |
| 6030 | GOST33 | 3.150 | | -1.84 | |
| 6190 | | | | | |
| | | 014 | | | |
| | normality | OK | | | |
| | n | 36 | | | |
| | outliers | 1 | | | |
| | mean (n) | 3.196 | | | |
| | st.dev. (n) | 0.0284 | | | |
| | R(calc.) | 0.079 | | | |
| | st.dev.(iis, lit. 16) | 0.0251 | | | 0 |
| | R(iis, lit. 16) | 0.070 | | | Compare R(D445:17) = 0.018, range 6 to 16 mm ² /s |
| | | | | | |

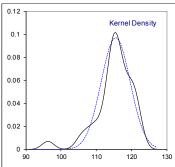




Determination of Viscosity Index on sample #18077;

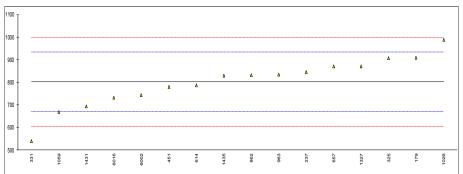
| lab | method | value | mark | z(targ) | iis calc. | | remarks |
|------|-------------------|---------------------|-------------|---------|-----------|---------|---|
| 178 | D2270 | 118 | | | 118.21 | | |
| 179 | D2270 | 113 | | | 113.19 | | |
| 225 | D2270 | 119.6 | ex | | 119.54 | ex | ecxcluded, outlier in kin. visc. 40°C |
| 237 | D2270 | 120.7 | E | | 121.79 | | calculation error |
| 325 | D2270 | 117.0 | | | 117.02 | | |
| 331 | | | | | | | |
| 349 | | | | | 115.64 | | |
| 360 | | | | | | | |
| 432 | D2270 | 118.7 | | | 118.65 | | |
| 451 | | | | | | | |
| 494 | D2270 | 116 | | | 116.27 | | |
| 496 | D2270 | 116 | | | 115.89 | | |
| 541 | D2270 | 105.5 | | | 105.47 | | |
| 603 | D2270 | 120.8 | | | 120.81 | | |
| 614 | D2270 | 107 | | | 107.05 | | |
| 633 | D2270 | 117.1 | | | 117.14 | | |
| 657 | | | | | | | |
| 663 | D2270 | 114.7 | | | 114.72 | | |
| 840 | D2270 | 115.8 | | | 115.79 | | |
| 862 | D2270 | 115 | | | 115.13 | | |
| 902 | D2270 | 116 | | | 116.10 | | |
| 912 | D2270 | 115 | | | 114.78 | | |
| 962 | | | | | | | |
| 963 | D2270 | 114 | | | 113.57 | | |
| 974 | D2270 | 113 | | | 112.88 | | |
| 1017 | D2270 | 114 | | | 113.62 | | |
| 1023 | | | | | 114.07 | | |
| 1026 | D2270 | 122 | E | | 116.99 | | calculation error |
| 1059 | ISO2909 | 114 | | | 114.48 | | |
| 1146 | D2270 | 115 | | | 115.17 | | |
| 1327 | D2270 | 111 | | | 111.28 | | |
| 1417 | D2270 | 116 | | | 116.19 | | |
| 1431 | D2270 | 118.7 | | | 118.69 | | |
| 1435 | D2270 | 121 | | | 121.32 | | |
| 1456 | D2270 | 121.72 | | | 121.72 | | |
| 1604 | | | _ | | 116.25 | | |
| 1875 | ISO2909 | 120 | E | | 120.70 | | calculation error |
| 1943 | ISO2909 | 96.3 | C,E,R(0.01) | | 95.66 | R(0.01) | first reported: 101.53, calculation error |
| 1966 | D2270 | 109.71 | E | | 108.04 | | calculation error |
| 6002 | ISO2909 | 115 | | | 115.15 | | |
| 6016 | 0.00707074 | | | | 117.32 | | |
| 6030 | GOST25371 | 109 | | | 108.82 | | |
| 6190 | | | | | | | |
| | normality | OK | | | OK | | |
| | normality | 31 | | | 35 | | |
| | n outliers | 1 (+1ex) | | | 1 (+1ex) | | |
| | mean (n) | 1 (+ Tex) 115.50 | | | 115.43 | ' | |
| | st.dev. (n) | 4.116 | | | 3.917 | | |
| | R(calc.) | 11.53 | | | 10.97 | | |
| | st.dev.(D2270:10) | (0.714) | | | (0.714) | | |
| | R(D2270:10) | (0.7 14) | | | (2) | | |
| | 11(02210.10) | (-) | | | (-) | | |

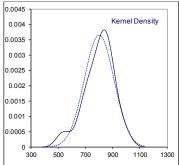




Determination of Oxidation Stability RPVOT on sample #18077; results in minutes

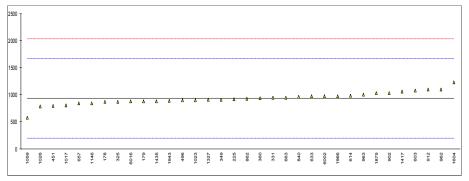
| lab | method | value | mark z(targ) | remarks |
|------|--------------------|-----------|--------------|---------|
| 178 | | | | |
| 179 | D2272 | 909 | 1.64 | |
| 225 | | | | |
| 237 | D2272 | 845 | 0.66 | |
| 325 | D2272 | 907 | 1.61 | |
| 331 | D2272 | 538 | -4.03 | |
| | DZZTZ | | | |
| 349 | | | | |
| 360 | | | | |
| 432 | 500-0 | | | |
| 451 | D2272 | 780 | -0.33 | |
| 494 | | | | |
| 496 | | | | |
| 541 | | | | |
| 603 | | | | |
| 614 | D2272 | 786 | -0.24 | |
| 633 | | | | |
| 657 | D2272 | 869 | 1.03 | |
| 663 | | | | |
| 840 | | | | |
| 862 | D2272 | 832 | 0.47 | |
| 902 | BLLTL | | | |
| 912 | | | | |
| 962 | | | | |
| | D2272 | | | |
| 963 | D2272 | 833 | 0.48 | |
| 974 | | | | |
| 1017 | | | | |
| 1023 | | | | |
| 1026 | D2272 | 987 | 2.83 | |
| 1059 | D2272 | 669 | -2.02 | |
| 1146 | | | | |
| 1327 | D2272 | 869 | 1.03 | |
| 1417 | | | | |
| 1431 | D2272 | 694 | -1.64 | |
| 1435 | D2272 | 830 | 0.44 | |
| 1456 | | | | |
| 1604 | | | | |
| 1875 | | | | |
| 1943 | | | | |
| 1966 | | | | |
| 6002 | D2272 | 744 | -0.88 | |
| 6016 | D2272 | 731.75 | -1.07 | |
| 6030 | DZZIZ | | -1.07 | |
| 6190 | | | | |
| 0190 | | | | |
| | n ormality | ou on oot | | |
| | normality | suspect | | |
| | n | 16 | | |
| | outliers | 0 | | |
| | mean (n) | 801.5 | | |
| | st.dev. (n) | 109.01 | | |
| | R(calc.) | 305.2 | | |
| | st.dev.(D2272:14a) | 65.44 | | |
| | R(D2272:14a) | 183.2 | | |
| | | | | |

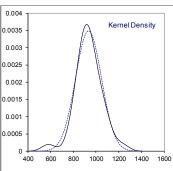




Determination of Water by KF on sample #18077; results in mg/kg

| lab | method | value | mark z(targ | remarks |
|------|---------------------|---------|-------------|---------|
| 178 | D6304-C | 867 | -0.18 | |
| 179 | D6304-C | 880 | -0.1 | |
| 225 | D6304-A | 914.44 | -0.0 | |
| 237 | | | | |
| 325 | D6304-C | 874 | -0.16 | |
| 331 | In house | 948.0 | 0.04 | |
| 349 | D6304-A | 913 | -0.0 | |
| 360 | D6304-A | 938.8 | 0.02 | |
| 432 | | | | |
| 451 | D6304-C | 798 | -0.37 | • |
| 494 | | | | |
| 496 | D6304-A | 900 | -0.09 | |
| 541 | | | | |
| 603 | D6304-C | 1077.7 | 0.40 | |
| 614 | D4928 | 988 | 0.15 | |
| 633 | D6304-C | 970 | 0.10 | |
| 657 | D6304-C | 840 | -0.2 | |
| 663 | D6304-C | 949.45 | 0.04 | |
| 840 | D6304-C | 963.4 | 0.08 | |
| 862 | D6304-C | 929 | -0.0 | |
| 902 | D6304-A | 1033 | 0.27 | |
| 912 | D6304-C | 1100 | 0.46 | |
| 962 | D6304-A | 1101 | 0.46 | |
| 963 | D6304-A | 1001 | 0.19 | |
| 974 | 2000171 | | | |
| 1017 | D6304-C | 803.25 | -0.36 | |
| 1023 | D6304-A | 900.6 | -0.09 | |
| 1026 | D6304-A | 788 | -0.40 | |
| 1059 | D6304Mod. | 580 | -0.97 | |
| 1146 | D6304-C | 845 | -0.24 | |
| 1327 | D6304-C | 912 | -0.06 | |
| 1417 | D6304-A | 1060 | 0.3 | |
| 1431 | | | | |
| 1435 | D6304-A | 883.1 | -0.14 | |
| 1456 | | | | |
| 1604 | D6304 | 1228.2 | 0.8 | |
| 1875 | ISO12937 | 1030 | 0.27 | |
| 1943 | EN60814 | 887.9 | -0.12 | |
| 1966 | EN60814 | 972.87 | 0.1 | |
| 6002 | ISO12937 | 970.23 | 0.10 | |
| 6016 | D6304-A | 877 | -0.1 | |
| 6030 | | | | |
| 6190 | | | | • |
| | | | | |
| | normality | not OK | | |
| | n | 34 | | |
| | outliers | 0 | | |
| | mean (n) | 933.06 | | |
| | st.dev. (n) | 114.404 | | |
| | R(calc.) | 320.33 | | |
| | st.dev.(D6304:16e1) | 365.140 | | |
| | R(D6304:16e1) | 1022.39 | | |
| | • | | | |

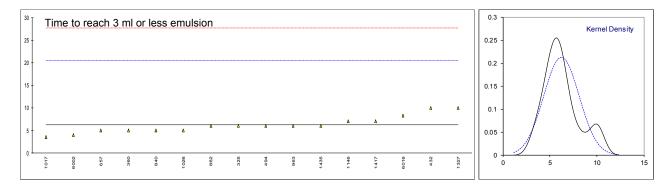


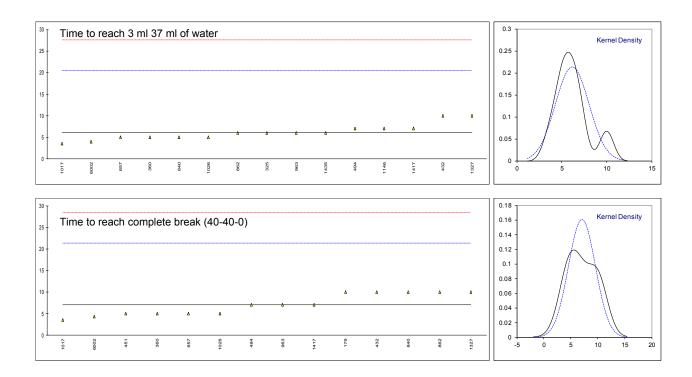


Determination of Water Separability at 54°C, distilled water on sample #18077; results in minutes

| | | time to | | time to | | time to | | | | |
|--------------|----------------|---------------------|--------------|----------------|------------|--------------------------|------|---------|-----------------|-------------------|
| | | reach 3 ml | | reach | | reach com- | | | toot | time test |
| lab | method | or less emulsion | mark z/tara) | 37 ml of water | mark 7/tor | plete break (40-40-0) | | =/toral | test aborted | time test aborted |
| | memou | | mark z(targ) | water | mark z(tar | <u></u> | mark | z(targ) | | |
| 178 179 | D1401 | | | | | | | 0.41 | NO | |
| 225 | D1401 | | | | | | | 0.41 | | |
| 237 | | | | | | | | | YES | 31.00 |
| 325 | D1401 | 6 | -0.03 | 6 | -0.02 | | | | YES | 30 |
| 331 | D1401 | | -0.03 | | -0.02 | | | | | |
| 349 | | | | | | | | | | |
| 360 | D1401 | 5 | -0.17 | 5 | -0.16 | | | -0.29 | NO | |
| 432 | D1401 | 10 | 0.53 | 10 | 0.54 | | | 0.41 | NO | |
| 451 | D1401 | | | | | | | -0.29 | | |
| 494 | D1401 | 6 | -0.03 | 7 | 0.12 | | | -0.01 | NO | |
| 496 | | | | | | | | | | |
| 541 | | | | | | | | | | |
| 603 | | | | | | | | | | |
| 614 | | | | | | | | | | |
| 633 | | | | | | | | | | |
| 657 | D1401 | 5 | -0.17 | 5 | -0.16 | 5 | | -0.29 | | |
| 663 | | | | | | | | | | |
| 840 | D1401 | 5 | -0.17 | 5 | -0.16 | 10 | | 0.41 | NO | |
| 862 | D1401 | 6 | -0.03 | 6 | -0.02 | 10 | | 0.41 | NO | 10 |
| 902 | | | | | | | | | | |
| 912 | | | | | | | | | | |
| 962 | | | | | | | | | | |
| 963 | D1401 | 6 | -0.03 | 6 | -0.02 | 7 | | -0.01 | NO | |
| 974 | | | | | | | | | | |
| 1017 | D1401 | 3.5 | -0.38 | 3.5 | -0.37 | | | -0.50 | NO | |
| 1023 | D4404 | | 0.47 | | | | | | | |
| 1026 | D1401 | 5 | -0.17 | 5 | -0.16 | | | -0.29 | NO | |
| 1059 1146 | D1401 | 7 | 0.11 | 7 | 0.12 | | | | | |
| 1327 | D1401 D1401 | 7 10 | 0.11 | 10 | 0.12 | | | 0.41 | NO | |
| 1417 | D1401 D1401 | 7 | 0.33 | 7 | 0.12 | | | -0.01 | NO | |
| 1431 | D1401 | <i>'</i> | 0.11 | | 0.12 | | | -0.01 | | |
| 1435 | ISO6614 | 6.01 | -0.03 | 6.01 | -0.02 | | | | | |
| 1456 | 1000014 | | | | | | | | | |
| 1604 | | | | | | | | | | |
| 1875 | | | | | | | | | | |
| 1943 | | | | | | | | | | |
| 1966 | | | | | | | | | | |
| 6002 | ISO6614 | 4.0 | -0.31 | 4.0 | -0.30 | 4.3 | | -0.39 | NO | |
| 6016 | D1401 | 8.32 | 0.29 | | | | | | NO | |
| 6030 | | | | | | | | | | |
| 6190 | | | | | | | | | | |
| | | | | | | | | | | |
| | normality | OK | | OK | | OK | | | | |
| | n | 16 | | 15 | | 14 | | | | |
| | outliers | 0 | | 0 | | 0 | | | | |
| | mean (n) | 6.24 | | 6.17 | | 7.06 | | | | |
| | st.dev. (n) | 1.875 | | 1.868 | | 2.488 | | | | |
| | R(calc.) | 5.25 | | 5.23 | | 6.97 | | | | |
| | st.dev.(D1401) | 7.143 | | 7.143 | | 7.143 | | | | |
| | R(D1401)* | 20 | | 20 | | 20 | | | | |







Determination of Water Separability at 54°C, distilled water on sample #18077; results in ml (cont.)

| | | volume oil | volume water | volume emulsion | test | |
|------------|---------|----------------|----------------|-----------------|--------|--|
| lab | method | phase | phase | phase | OK/NOK | remark |
| 178 | | | | | | |
| 179 | D1401 | 40 | 40 | 0 | OK | reported 10 min. to break |
| 225 | | | | | | |
| 237 | | 39 | 35 | 6 | OK | reported abort time of 31 min. |
| 325 | D1401 | 41 | 39 | 0 | OK | reported abort time of 30 min. |
| 331 | | | | | | |
| 349 | | | | | | |
| 360 | D1401 | 43 | 37 | 0 | OK | reported 5 min. to break |
| 432 | D1401 | 40 | 40 | 0 | OK | reported 10 min. to break |
| 451 | D1401 | 40 | 40 | 0 | OK | reported 5 min. to break |
| 494 | D1401 | 40 | 40 | 0 | OK | reported 7 min. to break |
| 496 | | | | | | |
| 541 | | | | | | |
| 603 | | | | | | |
| 614 | | | | | | |
| 633 | 54464 | | | | 014 | |
| 657 | D1401 | | | | OK | reported 5 min. to break |
| 663 | 54464 | | | | 014 | |
| 840 | D1401 | | | | OK | reported 10 min. to break |
| 862 | D1401 | 40 | 40 | 0 | OK | reported 10 min. to break |
| 902 | | | | | | |
| 912 | | | | | | |
| 962 | D1404 | 40 | 40 | | OK | namental 7 min to bundle |
| 963 974 | D1401 | 40 | 40 | 0 | OK | reported 7 min. to break |
| 1017 | D1401 | 40 | 40 | 0 | OK | reported 2.5 min. to break |
| 1017 | D1401 | 4 0 | 40 | | OK | reported 3.5 min. to break |
| 1023 | D1401 | 40 | 40 | 0 | OK | reported 5 min to break |
| 1020 | D1401 | 40 | 4 0 | · | OK | reported 5 min. to break |
| 1146 | D1401 | 40 | 37 | 3 | NOK* | did not report an abort time |
| 1327 | D1401 | 4 0 | <i></i> | J | OK | reported 10 min. to break |
| 1417 | D1401 | 40 | 40 | 0 | OK | reported 7 min. to break |
| 1431 | D1401 | | | | OIC | reported 7 min. to break |
| 1435 | ISO6614 | | | | NOK* | did not report a complete break or abort time |
| 1456 | 1000014 | | | | NOR | did not report a complete break or abort time |
| 1604 | | | | | | |
| 1875 | | | | | | |
| 1943 | | | | | | |
| 1966 | | | | | | |
| 6002 | ISO6614 | | | | OK | reported 4.3 min. to break |
| 6016 | D1401 | | | | NOK* | did not report a complete break or abort time |
| 6030 | | | | | | and the state of t |
| 6190 | | | | | | |

^{*} according to ASTM D1401 the amount of ml oil, ml water and ml emulsion should be reported as well as either the time the different volume requirements are met or when these are not reached, the time when the test is aborted (usually 30 minutes for tests at 54°C)

Determination of Demulsibility Characteristics, Steam on sample #18077; results in s en mL

| | | time to reach 20ml | | volume oil | | | |
|------|------------|----------------------|--------------|--------------|------|---------|---------|
| lab | method | of oil within 20 min | mark z(targ) | after 20 min | mark | z(tarq) | remarks |
| 178 | | | | | | | |
| 179 | | | | | | | |
| 225 | | | | | | | |
| 237 | | | | | | | |
| 325 | | | | | | | |
| 331 | | | | | | | |
| 349 | | | | | | | |
| 360 | | | | | | | |
| 432 | | | | | | | |
| 451 | IP19 | 120 | | | | | |
| 494 | | | | | | | |
| 496 | | | | | | | |
| 541 | | | | | | | |
| 603 | | | | | | | |
| 614 | | | | | | | |
| 633 | | | | | | | |
| 657 | | | | | | | |
| 663 | | | | | | | |
| 840 | | | | | | | |
| 862 | | | | | | | |
| 902 | | | | | | | |
| 912 | | | | | | | |
| 962 | | | | | | | |
| 963 | | | | | | | |
| 974 | | | | | | | |
| 1017 | | | | | | | |
| 1023 | | | | | | | |
| 1026 | | | | | | | |
| 1059 | | | | | | | |
| 1146 | | | | | | | |
| 1327 | | | | | | | |
| | IP19 | 120 | | 20 | | | |
| 1431 | 11 10 | | | | | | |
| 1435 | | | | | | | |
| 1456 | | | | | | | |
| 1604 | | | | | | | |
| 1875 | | | | | | | |
| 1943 | | | | | | | |
| 1966 | | | | | | | |
| 6002 | PN-C04110 | 76 | | 20 | | | |
| 6016 | 111-00-110 | 70 | | | | | |
| 6030 | | | | | | | |
| 6190 | | | | | | | |
| 0190 | | 1 | | 1 - | | | |
| | n | 3 | | 2 | | | |
| | mean (n) | 76-120 | | 20 | | | |
| | carr (11) | . 5 120 | | _0 | | | |

Determination of Water separation ability, Steam, time to reach the $55\,$ mm measuring point (oil-water phase) on sample #18077; results in s

| lab | method | value | mark z(targ) | remarks |
|--------------|-----------|-------|--------------|-----------|
| 178 | ilietilou | | | IGIIIQINS |
| 179 | | | | |
| 225 | | | | |
| 237 | | | | |
| 325 | | | | |
| 331 | | | | |
| 349 | | | | |
| 360 | | | | |
| 432 | | | | |
| 451 | | | | |
| 494 | | | | |
| 496 | DIN51589 | 79 | | |
| 541 | | | | |
| 603 | | | | |
| 614 | | | | |
| 633 | | | | |
| 657 | | | | |
| 663 | | | | |
| 840 | | | | |
| 862 | | | | |
| 902 | | | | |
| 912 | | | | |
| 962 | | | | |
| 963 | | | | |
| 974 | | | | |
| 1017 | | | | |
| 1023 | | | | |
| 1026 | | | | |
| 1059 | | | | |
| 1146 | | | | |
| 1327 | | | | |
| 1417 | | | | |
| 1431 | | | | |
| 1435 | | | | |
| 1456 | | | | |
| 1604 | | | | |
| 1875 | | | | |
| 1943 | | | | |
| 1966 | | | | |
| 6002 | | | | |
| 6016 | | | | |
| 6030 6190 | | | | |
| 0190 | | | | |

Determination of Level of Contamination on sample #18077; results in counts per ml

| lab | method | ≥ 4 µm(c) | mark | z(targ) | ≥ 6 µm(c) | mark | z(targ) | ≥ 14 µm(c) | mark | z(targ) |
|------|-------------------|-----------|------|---------|-----------|------|---------|------------|-------|---------|
| 178 | INH-1184 | 15301 | | -0.60 | 2355 | | -1.78 | 13 | ex | -1.92 |
| 179 | D7647 | 21824 | С | 0.19 | 3831 | С | -0.59 | 123 | ex, C | -0.63 |
| 225 | D1 0-1 | 21027 | 9 | | | J | -0.55 | | CA, O | -0.03 |
| | | | | | | | | | | |
| 237 | | | | | | | | | | |
| 325 | | | | | | | | | | |
| 331 | | | | | | | | | | |
| 349 | | | | | | | | | | |
| 360 | ISO4406 | 25578 | | 0.65 | 4813 | | 0.20 | 169 | | -0.09 |
| 432 | | | | | | | | | | |
| 451 | ISO11500 | 23905 | | 0.45 | 5247 | | 0.55 | 55 | | -1.43 |
| 494 | | | | | | | | | | |
| 496 | D7647 | 25610 | | 0.66 | 5891 | | 1.07 | 238 | | 0.72 |
| 541 | B1041 | | | | | | | | | |
| 603 | | | | | | | | | | |
| | 1004407 | 0.4000 | | 0.50 | 0704 | | 4.75 | | | 4.00 |
| 614 | ISO4407 | 24332 | | 0.50 | 6724 | | 1.75 | 23 | | -1.80 |
| 633 | D7647 | 32847 | | 1.54 | 5121 | | 0.45 | 110 | | -0.78 |
| 657 | ISO4406 | 3953 | | -1.99 | 1826 | | -2.21 | 220 | | 0.51 |
| 663 | D7647 | 4787 | | -1.89 | 1856 | | -2.18 | 177 | | 0.01 |
| 840 | | 23455.1 | | 0.39 | 6254.4 | | 1.37 | 256.3 | | 0.94 |
| 862 | ISO11500 | 23253 | | 0.37 | 4110 | | -0.36 | 122 | | -0.64 |
| 902 | D7647 | 13668 | | -0.80 | 3339 | | -0.99 | 76.9 | | -1.17 |
| 912 | 21011 | | | | | | | | | |
| 962 | | | | | | | | | | |
| | D7047 | | | | | | | | | |
| 963 | D7647 | 5075 | | -1.86 | 1456 | | -2.51 | 37 | | -1.64 |
| 974 | | | | | | | | | | |
| 1017 | ISO11500 | 34879.99 | | 1.79 | 9308.45 | | 3.84 | 350.49 | | 2.04 |
| 1023 | | | | | | | | | | |
| 1026 | | | | | | | | | | |
| 1059 | D7647 | 1922 | ex | -2.24 | 3596 | | -0.78 | 84 | | -1.09 |
| 1146 | ISO11500 | 2580 | ex | -2.16 | 571 | ex | -3.22 | 20 | ex | -1.84 |
| 1327 | D7647 | 23230 | | 0.37 | 4508 | | -0.04 | 237 | | 0.71 |
| 1417 | 2.0 | | | | | | | | | |
| 1431 | ISO4407 | 26342.28 | | 0.75 | 6043.32 | | 1.20 | 245.60 | | 0.81 |
| 1435 | 1004407 | 31557.10 | | 1.39 | 8062.60 | | 2.83 | 320.83 | | 1.70 |
| | 1004406 | | | | | | | 439.4 | | |
| 1456 | ISO4406 | 36259 | | 1.96 | 10883.5 | | 5.11 | | | 3.09 |
| 1604 | D7647 | 16623 | | -0.44 | 3552 | | -0.81 | 113 | | -0.75 |
| 1875 | | | | | | | | | | |
| 1943 | | 29766.54 | ex | 1.17 | 3075.14 | | -1.20 | 194.77 | ex | 0.21 |
| 1966 | | | | | | | | | | |
| 6002 | D7596 | 1975.8 | | -2.24 | 802.2 | | -3.04 | 120.1 | | -0.66 |
| 6016 | D7596 | 12586 | | -0.94 | 2973 | | -1.28 | 140 | | -0.43 |
| 6030 | - | | | | | | | | | |
| 6190 | ISO11500 | 18138.06 | | -0.26 | 3828.06 | | -0.59 | 171.70 | | -0.06 |
| 0100 | 1000 | .0.100.00 | | 0.20 | 3020.00 | | 0.00 | .,, 0 | | 0.00 |
| | normality | OK | | | OK | | | OK | | |
| | normality | | | | | | | | | |
| | n ti | 22 | | | 24 | | | 21 | | |
| | outliers | 0 (+3ex) | | | 0(+1ex) | | | 0(+4ex) | | |
| | mean (n) | 20235.4 | | | 4560.65 | | | 176.49 | | |
| | st.dev. (n) | 10058.99 | | | 2467.310 | | | 107.930 | | |
| | R(calc.) | 28165.2 | | | 6908.47 | | | 302.20 | | |
| | st.dev.(D7647:10) | 8166.44 | | | 1237.891 | | | 85.094 | | |
| | R(D7647:10) | 22866.0 | | | 3466.10 | | | 238.26 | | |
| | 11(27047.10) | 000.0 | | | 5 100.10 | | | 200.20 | | |

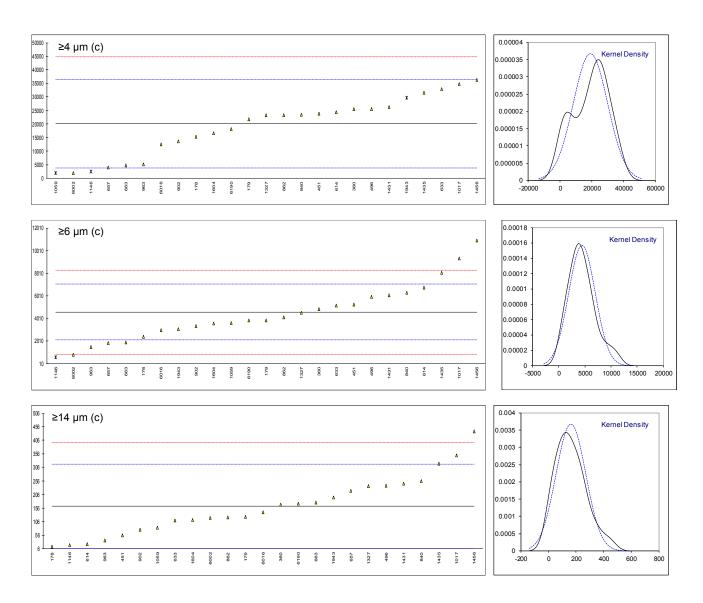
Lab 178 the test result for \ge 14 μ m was excluded for the test result in counts/ml did not match the ISO scale number

Lab 179 first reported for ≥4 μm: 2409460, for for ≥6 μm: 343604 and for for ≥14 μm: 17417, the test result for ≥14 μm was excluded for the test result in counts/ml did not match the ISO scale number

Lab 1059 the test result for ≥4 µm was excluded for the test result in counts/ml did not match the ISO scale number

Lab 1146 all test results were excluded for the test result in counts/ml did not match the ISO scale numbers

Lab 1943 the test results for≥4 µm and ≥14 µm were excluded for the test result in counts/ml did not match the ISO scale numbers



Determination of Level of Contamination on sample #18077; results in ISO 4406 scale numbers

| lab | method | ≥ 4 µm(c) | mark | z(targ) | ≥ 6 µm(c) | mark | z(targ) | ≥ 14 µm(c) | mark | z(targ) |
|------|-------------------|-----------|------------|---------|-----------|------|---------|------------|------|---------|
| 178 | ISO4406 | 21 | | -1.20 | 18 | | -2.94 | 12 | ex | -3.44 |
| 179 | ISO4406 | 22 | | 0.45 | 19 | | -0.60 | 15 | ex | 0.76 |
| 225 | | | | | | | | | - | |
| 237 | | | | | | | | | | |
| 325 | | | | | | | | | | |
| 331 | | | | | | | | | | |
| | | | | | | | | | | |
| 349 | 1004400 | | | | | | | 4 | | |
| 360 | ISO4406 | 22 | | 0.45 | 19 | | -0.60 | 15 | | 0.76 |
| 432 | | | | | | | | | | |
| 451 | ISO4406 | 22 | | 0.45 | 20 | | 1.73 | 13 | | -2.04 |
| 494 | | | | | | | | | | |
| 496 | ISO4406 | 22 | | 0.45 | 20 | | 1.73 | 15 | | 0.76 |
| 541 | | | | | | | | | | |
| 603 | | | | | | | | | | |
| 614 | ISO4406 | 22 | | 0.45 | 20 | | 1.73 | 12 | | -3.44 |
| 633 | ISO4406 | 22 | | 0.45 | 20 | | 1.73 | 14 | | -0.64 |
| 657 | ISO4406 | 19 | C, R(0.01) | -4.49 | 18 | С | -2.94 | 15 | С | 0.76 |
| 663 | ISO4406 | 19 | R(0.01) | -4.49 | 18 | | -2.94 | 15 | | 0.76 |
| 840 | | 22 | (****) | 0.45 | 20 | | 1.73 | 15 | | 0.76 |
| 862 | ISO11500 | 22 | | 0.45 | 19 | | -0.60 | 14 | | -0.64 |
| 902 | ISO4406 | 21 | | -1.20 | 19 | | -0.60 | 13 | | -2.04 |
| 912 | 1004400 | | | -1.20 | | | -0.00 | | | -2.04 |
| 962 | | | | | | | | | | |
| 963 | ISO4406 | 20 | | -2.84 | 18 | | -2.94 | 12 | | -3.44 |
| 974 | 1304400 | | | -2.04 | | | -2.94 | | | -3.44 |
| | ISO11500 | 22 | | 0.45 | 20 | | 1.73 | 16 | | 2.16 |
| 1017 | | | | | | | | | | |
| 1023 | ISO4406 | 22 | 0 | 0.45 | 20 | | 1.73 | 14 | _ | -0.64 |
| 1026 | ISO4406 | 22 | С | 0.45 | 20 | | 1.73 | 16 | С | 2.16 |
| 1059 | ISO4406 | 21 | ex | -1.20 | 19 | | -0.60 | 14 | | -0.64 |
| 1146 | ISO4406 | 22 | ex | 0.45 | 20 | ex | 1.73 | 15 | ex | 0.76 |
| 1327 | ISO4406 | 22 | | 0.45 | 19 | | -0.60 | 15 | | 0.76 |
| 1417 | ISO4406 | 23 | | 2.10 | 20 | | 1.73 | 15 | | 0.76 |
| 1431 | ISO4406 | 22 | | 0.45 | 20 | | 1.73 | 15 | | 0.76 |
| 1435 | ISO4406 | 22 | | 0.45 | 20 | | 1.73 | 16 | | 2.16 |
| 1456 | ISO4406 | 22 | | 0.45 | 21 | | 4.06 | 16 | | 2.16 |
| 1604 | D7647 | 21 | | -1.20 | 19 | | -0.60 | 14 | | -0.64 |
| 1875 | | | | | | | | | | |
| 1943 | ISO4406 | 21 | ex | -1.20 | 19 | | -0.60 | 14 | ex | -0.64 |
| 1966 | | | | | | | | | | |
| 6002 | ISO4406 | 18 | R(0.01) | -6.14 | 17 | | -5.27 | 14 | | -0.64 |
| 6016 | ISO4406 | 21 | | -1.20 | 19 | | -0.60 | 14 | | -0.64 |
| 6030 | | | | | | | | | | |
| 6190 | ISO4406 | 21 | | -1.20 | 19 | | -0.60 | 15 | | 0.76 |
| | normality | suspect | | | ОК | | | OK | | |
| | n | 22 | | | 27 | | | 24 | | |
| | outliers | 3 (+3ex) | | | 0 (+1ex) | | | 0 (+4ex) | | |
| | mean (n) | 21.7 | | | 19.3 | | | 14.5 | | |
| | st.dev. (n) | 0.63 | | | 0.90 | | | 1.14 | | |
| | R(calc.) | 1.8 | | | 2.5 | | | 3.2 | | |
| | st.dev.(D7647:10) | 0.61 | | | 0.43 | | | 0.71 | | |
| | R(D7647:10) | 1.7 | | | 1.2 | | | 2 | | |

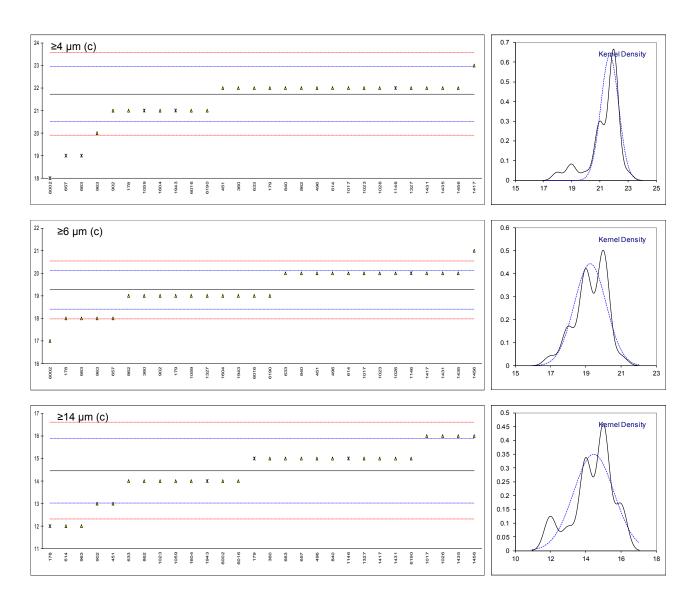
Lab 178 the test result for \geq 14 μ m was excluded for the test result in counts/ml did not match the ISO scale number Lab 179 the test result for \geq 14 μ m was excluded for the test result in counts/ml did not match the ISO scale number

Lab 657 first reported for≥4 μm: 3953, for for ≥6 μm: 1826 and for for ≥14 μm: 220

Lab 1026 first reported for ≥4 μm: 21, for for ≥6 μm: 18 and for for ≥14 μm: 9
Lab 1059 the test result for ≥4 μm was excluded for the test result in counts/ml did not match the ISO scale number

Lab 1146 all test results were excluded for the test result in counts/ml did not match the ISO scale numbers

Lab 1943 the test results for≥4 µm and ≥14 µm were excluded for the test result in counts/ml did not match the ISO scale numbers



APPENDIX 2

Number of participants per country

- 1 lab in ARGENTINA
- 2 labs in AUSTRALIA
- 1 lab in AUSTRIA
- 3 labs in BELGIUM
- 1 lab in BULGARIA
- 2 labs in CHINA, People's Republic
- 1 lab in COTE D'IVOIRE
- 1 lab in FRANCE
- 2 labs in GEORGIA
- 3 labs in GERMANY
- 1 lab in GREECE
- 1 lab in INDIA
- 1 lab in KAZAKHSTAN
- 1 lab in LATVIA
- 1 lab in MALAYSIA
- 2 labs in NETHERLANDS
- 1 lab in NIGERIA
- 1 lab in NORWAY
- 1 lab in PHILIPPINES
- 1 lab in POLAND
- 1 lab in ROMANIA
- 2 labs in SAUDI ARABIA
- 1 lab in SINGAPORE
- 1 lab in SLOVENIA
- 2 labs in SPAIN
- 1 lab in THAILAND
- 1 lab in TURKEY
- 1 lab in UNITED ARAB EMIRATES
- 2 labs in UNITED KINGDOM
- 2 labs in UNITED STATES OF AMERICA
- 1 lab in VIETNAM

APPENDIX 3

Abbreviations:

C = final test result after checking of first reported suspect test result

D(0.01) = outlier in Dixon's outlier test

D(0.05) = straggler in Dixon's outlier test

G(0.01) = outlier in Grubbs' outlier test

G(0.05) = straggler in Grubbs' outlier test

DG(0.01) = outlier in Double Grubbs' outlier test

DG(0.05) = straggler in Double Grubbs' outlier test

R(0.01) = outlier in Rosner's outlier test

R(0.05) = straggler in Rosner's outlier test

ex = test result excluded from the statistical evaluation

U = reported test result in a different unit

W = test result withdrawn on request of the participants

fr. = first reported test result

n.a. = not applicablen.e. = not evaluatedn.d. = not detected

SDS = Material Safety Data Sheet

Literature:

- 1 iis Interlaboratory Studies, Protocol for the Organization, Statistics and Evaluation, March 2017
- 2 ASTM E178:89
- 3 ASTM E1301:89
- 4 ISO 5725:86
- 5 ISO 5725, parts 1-6, 1994
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